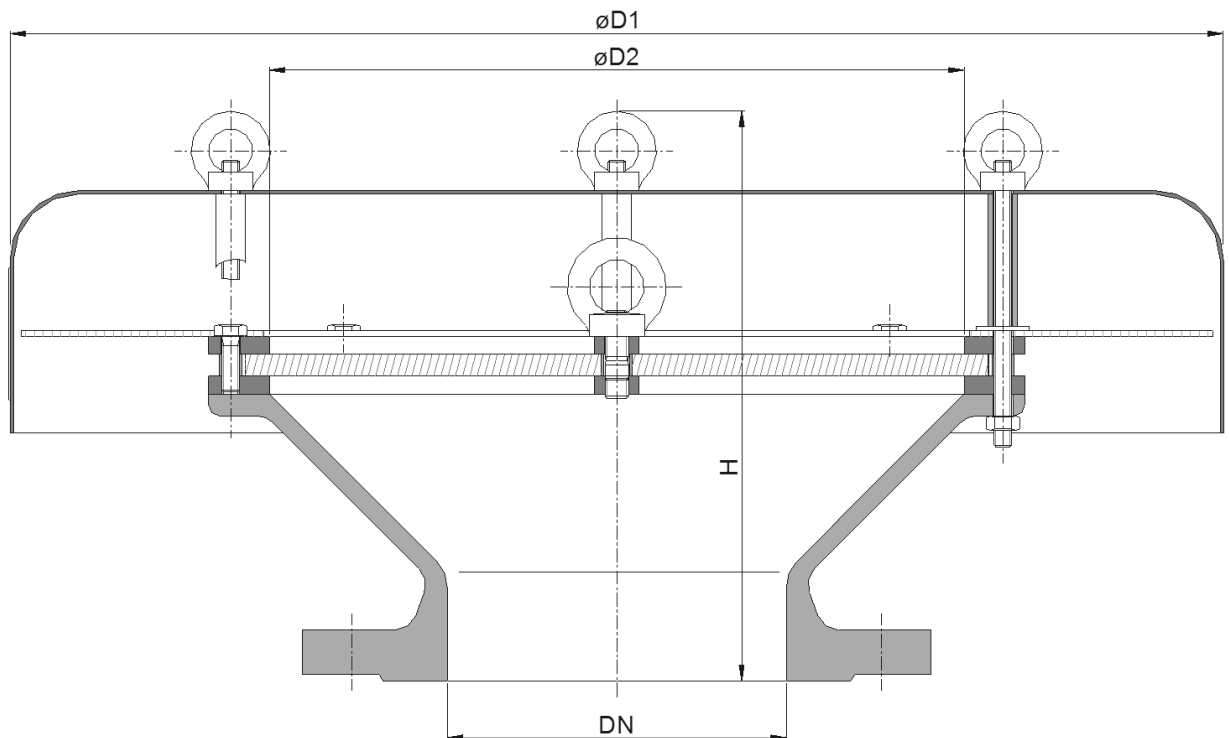
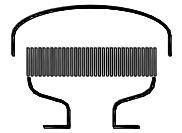


Hooded Tank Vent KITO® VH-...-IIB3



Type examination certificate to DIN EN ISO 16852

CE -designation in accordance to ATEX-Guideline 94/9/EC

DN	ANSI	D1	D2	H		kg*
50 PN 16	2"	285	110	170		7.3
80 PN 16	3"	330	150	180		11
100 PN 16	4"	405	185	220		15
150 PN 16	6"	550	315	260		29.9
200 PN 10	8"					31.5
250 PN 10	10"	600	395	355		62.5
300 PN 10	12"			350	396	62
350 PN 10	14"	800	595	405	464	88
400 PN 10	16"			400	455	103
450 PN 10	18"	1000	700	-		489
500 PN 10	20"			415	485	130
600 PN 10	24"	1200	800	485	558	192
700 PN 10	-	1400	1000	520	-	265
800 PN 10	-	1600	1210	560	-	345

Dimensions in mm

* weight refers to the standard design



Example to order :

KITO® VH-300-IIB3

(design with flange connection DN 300)

performance curves: B 0.6 N

Design subject to change

Standard design

housing	: cast steel 1.0619 (> DN 350 steel), stainless cast steel 1.4408 (> DN 350 stainless steel mat. no.1.4571)
KITO® flame arrester element	: interchangeable
KITO® casing	: steel, stainless steel mat. no. 1.4571
KITO® grid	: stainless steel mat. no. 1.4310, 1.4571
weather hood	: stainless steel mat. no. 1.4301, 1.4571
protective screen	: stainless steel mat. no. 1.4301 (not for DN 50-100)
flange connection	: DIN EN 1092-1 form B1 ANSI 150 lbs. RF

Application

As breather/venting safety device incorporating an explosion proof flame arrester element for installation on top of storage tanks, tank access covers or breather pipes. The breather allows the unimpeded flow of gases out to atmosphere and air into the tank/pipe thereby preventing vacuum locks whilst ensuring provision of a permanent and reliable protection against any flashback into the tank/pipe.

This device is not permitted to be installed in enclosed areas.

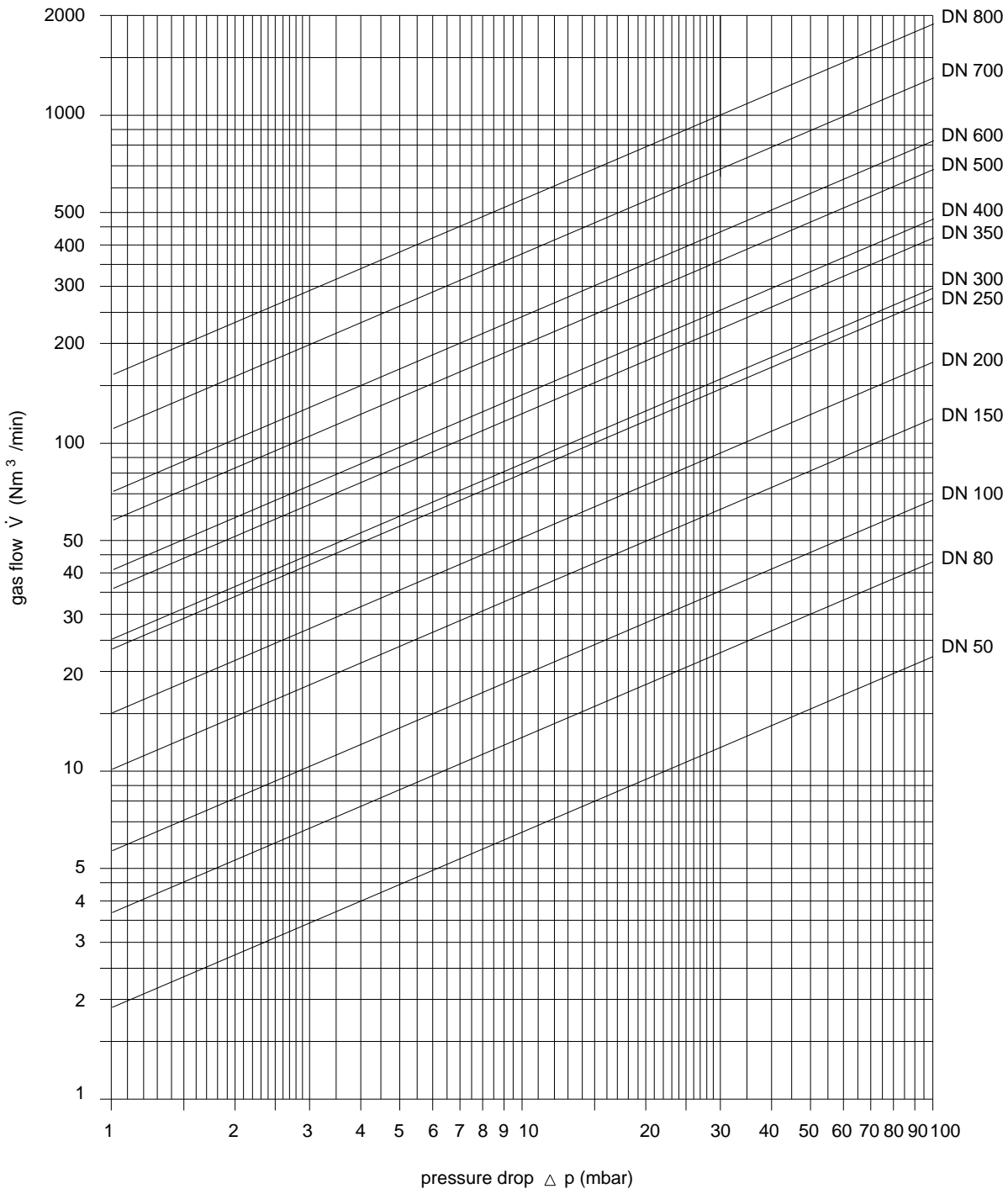
Approved for all materials of the explosion group IIB3 with a maximum experimental safe gap (MESG) ≥ 0.65.



Hooded Tank Vent
KITO® VH-...IB3
B 6 N

Flow capacity V based on air of a density $\rho = 1.29 \text{ kg/m}^3$ at $T = 273 \text{ K}$ and atmospheric pressure $p = 1.013 \text{ mbar}$. For other gases the flow can be approximately calculated by

$$\dot{V} = \dot{V}_b \cdot \sqrt{\frac{\rho_b}{1.29}} \quad \text{or} \quad \dot{V}_b = \dot{V} \cdot \sqrt{\frac{1.29}{\rho_b}}$$



Design subject to change